

APPENDIX A

% BEGINNING OF PSEUDO CODE

5 % compute scale factor A, and time constants a, b from physical system
 % parameters

$$A = V_{\max} * K_t / (R_e * R_m + K_t * K_b) * l * k;$$

10
$$p1 = 1/J_m/I_e * (-I_e * R_m - R_e * J_m + \sqrt{I_e^2 * R_m^2 - 2 * R_e * R_m * I_e * J_m + R_e^2 * J_m^2 - 4 * K_t * K_b * I_e * J_m}) / 2;$$

$$p2 = 1/J_m/I_e * (-I_e * R_m - R_e * J_m - \sqrt{I_e^2 * R_m^2 - 2 * R_e * R_m * I_e * J_m + R_e^2 * J_m^2 - 4 * K_t * K_b * I_e * J_m}) / 2;$$

15
$$a = \max(-p1, -p2)$$

$$b = \min(-p1, -p2)$$

% make initial guesses for step durations

20
$$et1 = 1;$$

$$et2 = .005;$$

$$et3 = 1;$$

% set maximum iteration count

25
$$N_{\max} = 1000;$$

for j = 1:Nmax

 % save old values of step time intervals

30
$$et3_{\text{old}} = et3;$$



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et2old = et2;
et1old = et1;

% iterate for switch times using fixed voltage level Vmax
5
    et3 = -log(1.0 / 2.0 - exp(-et1 * a) / 2 + exp(-et2 * a)) / a;
    et2 = 1/b * log(2.0) + 3 * et3 - 1/b * log(2 * exp(1/A * b * X) *
        exp(et3 * b) - sqrt( 4.0) * sqrt(exp(1/A * b * X)) * exp(et3 * b)
        * sqrt(exp(1/A * b * X)+exp(et3 * b)^2 - 2 * exp(et3 * b)));
10    et1 = - (-2 * A * et2 + 2 * A * et3 - X) / A;

    if norm([et3old - et3 et2old - et2 et1old - et1], inf) <= eps * 2
        break
    end
15    if j==Nmax
        error(['error - failure to converge after ', num2str(Nmax), '
            iterations'])
    end
end
20
% round up pulse duration to nearest sample interval,
% convert to intervals between steps to make sure that voltage
% requirements will not increase (beyond Vmax).

25    dt1=ceil((et1 - et2) / dt) * dt;
    dt2=ceil((et2 - et3) / dt) * dt;
    dt3=ceil((et3) / dt) * dt;

    et123 = [et1, et2, et3]
30    % convert back to total step duration.

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$$et1 = dt1 + dt2 + dt3;$$

$$et2 = dt2 + dt3;$$

$$et3 = dt3;$$

5 % In the following, the original constraints equations involving XF1, XF2,
 % and XF3 have been modified to include a variable voltage level applied at
 % each step (instead of the fixed maximum (+/-) Vmax).

 % The original equations for XF1, XF2, and XF3 follow:

10 % $XF_1(t_{end}) = V_0 F_1(t_{end} - t_0) - 2V_0 F_1(t_{end} - t_1) + 2V_0 F_1(t_{end} - t_2)$

 % $XF_2(t_{end}) = V_0 F_2(t_{end} - t_0) - 2V_0 F_2(t_{end} - t_1) + 2V_0 F_1(t_{end} - t_2)$

 % $XF_3(t_{end}) = V_0 F_3(t_{end} - t_0) - 2V_0 F_2(t_{end} - t_1) + 2V_0 F_1(t_{end} - t_2)$

 % And the modified equation including adjustable relative levels of voltage

15 % L1, L2 and L3 are:

 % $XF_1(t_{end}) = L_1 V_0 F_1(t_{end} - t_0) - L_2 V_0 F_1(t_{end} - t_1) + L_3 V_0 F_1(t_{end} - t_2)$

 % $XF_2(t_{end}) = L_1 V_0 F_2(t_{end} - t_0) - L_2 V_0 F_2(t_{end} - t_1) + L_3 V_0 F_1(t_{end} - t_2)$

 % $XF_3(t_{end}) = L_1 V_0 F_3(t_{end} - t_0) - L_2 V_0 F_2(t_{end} - t_1) + L_3 V_0 F_1(t_{end} - t_2)$

20 % And the corresponding constraint equations are:

 % $XF_1(t_{end}) = \text{Finalpos}$

 % $XF_2(t_{end}) = 0$

 % $XF_3(t_{end}) = 0$

25 % Where all of the times indicated have discrete values, e.g. corresponding to
 % the controller update rate.

 % It should be noted that after the digital switch times are fixed, the constraint
 % equations derived from the equations above form a linear set of equations in

30 % the unknown relative voltage levels L1, L2 and L3 and any standard linear

% method can be used to solve for the relative voltage levels. In the equations
 % for (L1, L2 and L3) that follow, the solution was obtained by algebraic
 % means (and are not particularly compact.)

5 % compute new relative voltage step levels

% L1, L2 and L3 are nominally assigned to "1", "-2" and "+2", respectively

$$s1 = X * (\exp(-et3 * b) * \exp(-et2 * a) + \exp(-et3 * a) + \exp(-et2 * b) - \exp(-et2 * b) * \exp(-et3 * a) - \exp(-et2 * a) - \exp(-et3 * b));$$

$$10 \quad s2 = 1 / (et2 * \exp(-et1 * b) * \exp(-et3 * a) + \exp(-et2 * b) * et3 * \exp(-et1 * a) - et2 * \exp(-et3 * a) - et2 * \exp(-et1 * b) - et3 * \exp(-et1 * a) - \exp(-et2 * b) * et3 + \exp(-et3 * b) * et1 * \exp(-et2 * a) + \exp(-et3 * a) * et1 + \exp(-et2 * b) * et1 - \exp(-et2 * b) * et1 * \exp(-et3 * a) - et3 * \exp(-et1 * b) * \exp(-et2 * a) - \exp(-et2 * a) * et1 - \exp(-et3 * b) * et1 - \exp(-et3 * b) * et2 * \exp(-et1 * a) + et3 * \exp(-et1 * b) + et2 * \exp(-et1 * a) + \exp(-et3 * b) * et2 + et3 * \exp(-et2 * a)) / A;$$

$$L1 = s1 * s2;$$

20

$$s1 = 1 / (et2 * \exp(-et1 * b) * \exp(-et3 * a) + \exp(-et2 * b) * et3 * \exp(-et1 * a) - et2 * \exp(-et3 * a) - et2 * \exp(-et1 * b) - et3 * \exp(-et1 * a) - \exp(-et2 * b) * et3 + \exp(-et3 * b) * et1 * \exp(-et2 * a) + \exp(-et3 * a) * et1 + \exp(-et2 * b) * et1 - \exp(-et2 * b) * et1 * \exp(-et3 * a) - et3 * \exp(-et1 * b) * \exp(-et2 * a) - \exp(-et2 * a) * et1 - \exp(-et3 * b) * et1 - \exp(-et3 * b) * et2 * \exp(-et1 * a) + et3 * \exp(-et1 * b) + et2 * \exp(-et1 * a) + \exp(-et3 * b) * et2 + et3 * \exp(-et2 * a)) * X;$$

25

$$s2 = (\exp(-et2 * b) * \exp(-et1 * a) - \exp(-et1 * a) - \exp(-et2 * b) - \exp(-et1 * b) * \exp(-et2 * a) + \exp(-et1 * b) + \exp(-et2 * a)) / A;$$

30

L3 = s1*s2;

s1 = exp(-et1 * a) - exp(-et3 * a) + exp(-et3 * b) - exp(-et1 * b) -
exp(-et3 * b) * exp(-et1 * a) + exp(-et1 * b) * exp(-et3 * a);

5 s2 = X / (et2 * exp(-et1 * b) * exp(-et3 * a) + exp(-et2 * b) * et3 *
exp(-et1 * a) - et2 * exp(-et3 * a) - et2 * exp(-et1 * b) - et3 *
exp(-et1 * a) - exp(-et2 * b) * et3 + exp(-et3 * b) * et1 * exp(-et2 * a)
+ exp(-et3 * a) * et1 + exp(-et2 * b) * et1 - exp(-et2 * b) * et1 *
exp(-et3 * a) - et3 * exp(-et1 * b) * exp(-et2 * a) - exp(-et2 * a) * et1 -
10 exp(-et3 * b) * et1 - exp(-et3 * b) * et2 * exp(-et1 * a) + et3 *
exp(-et1 * b) + et2 * exp(-et1 * a) + exp(-et3 * b) * et2 + et3 *
exp(-et2 * a)) / A;

L2 = s1 * s2;

15

% convert accumulated voltage steps to sequential voltage level

V1 = Vmax * (L1);

V2 = Vmax * (L1 + L2);

V3 = Vmax * (L1 + L2 + L3);

20

% END OF PSEUDO CODE